

PROFESSIONAL LINE - Subwoofer 18SW1P / 18SW1P-SLF*

The 18SW1P / 18SW1P-SLF* is a high power 18" professional subwoofer specially designed to reproduce sound at the very low end of the audio spectrum.

In order to achieve a perfect performance in this very demanding region of low frequencies, the 18SW1P / 18SW1P-SLF* is capable of handling up to 800 W RMS or 1,600 W (Musical Program).

A bumped bottom plate assures a compatible maximum displacement and the extended pole piece keeps the magnetic field linearity in order to avoid distortion; it also improves the heat transfer.

The magnet assembly was designed with the assistance of a Finite

Element Analysis (FEA) software in order to ensure optimization.

A 4" (100 mm) voice coil wound in a fiberglass former with flat copper clad aluminum wire drives the moving assembly.

A non-pressed long fiber pulp cone has the necessary stiffness to withstand the tremendous accelerating forces involved and is properly centered by two counteracting polyamide fiber spiders.

An triple cooling system consisting of a long discrete state but the

An triple cooling system consisting of a large diameter center hole surrounded by six smaller holes (directly cooling the gap) and six frame windows (cooling the air trapped between the two spiders) are responsible for an efficient heat transfer mechanism.

A highly reinforced aluminum injected frame is effective in absorbing mechanical shocks and acts as a heat sink without interfering with the magnetic

*18SW1P-SLF: Product without Selenium logo printed on the dust cap.

SPECIFICATIONS

Nominal diameter	mm (in)
Nominal impedance8	
Minimum impedance @ 112 Hz7.2	
Power handling	
Musical program ¹ 1,600	W
AES ²	W
Sensitivity (2.83V@1m) averaged from 80 to 250 Hz 97	dB SPL
Power compression @ 0 dB (nom.power)3.3	dB
Power compression @ -3 dB (nom.power)/22.8	dB
Power compression @ -10 dB (nom.power)/100.7	dB
Frequency response @ -10 dB 30 to 2,500	Hz

¹ Power handling specifications refer to normal speech and/or music program material, reproduced by an amplifier producing no more than 5% distortion. Power is calculated as true RMS voltage squared divided by the nominal impedance of the loudspeaker.
² AES Standard (60 - 600 Hz).

THIFLE-SMALL PARAMETERS

INIELE-SWALL PARAWETERS	
Fs37	Hz
Vas	I (ft ³)
Qts	
Qes	
Qms11.45	
o (half space)	%
Sd	m² (in²)
Vd (Sd x Xmax)	cm³ (iń³)
Xmax (max. excursion (peak) with 10% distortion) 9.3 (0.37)	mm (in)
Xlim (max.excursion (peak) before physical damage)25.0 (0.98)	mm (in)
Atmospheric conditions at TS parameter measurements:	
Temperature	°C (°F)
Atmospheric pressure	mb` ´

Thiele-Small parameters are measured after a 2-hour power test using half AES power .

Humidity......59

ADDITIONAL PARAMETERS

L	Tm
Flux density	T
Voice coil diameter	mm (in)
Voice coil winding length	m (ft)
Wire temperature coefficient of resistance () 0.00372	1/°C
Maximum voice coil operating temperature275 (527)	°C (°F)
vc (max.voice coil operating temp./max.power) 0.34 (0.66)	°C/W(°F/W)
Hvc (voice coil winding depth)	mm (in)
Hag (air gap height)	mm (iní)
Re	,
Mms	g (lb)
Cms	m/Ń
Rms3.3	kg/s
	· ·
NON-LINEAR PARAMETERS	
Le @ Fs (voice coil inductance @ Fs)11.073	
Le & 13 (voice con inductance & 13)	mΗ
Le @ 1 kHz (voice coil inductance @ 1 kHz) 2.549	mH mH
Le @ 1 kHz (voice coil inductance @ 1 kHz) 2.549	mH
Le @ 1 kHz (voice coilinductance @ 1 kHz) 2.549 Le @ 20 kHz (voice coilinductance @ 20 kHz) 0.674	mH
Le @ 1 kHz (voice coil inductance @ 1 kHz) 2.549 Le @ 20 kHz (voice coil inductance @ 20 kHz) 0.674 Red @ Fs 0.81	mH
Le @ 1 kHz (voice coil inductance @ 1 kHz) 2.549 Le @ 20 kHz (voice coil inductance @ 20 kHz) 0.674 Red @ Fs 0.81 Red @ 1 kHz 10.10	mH
Le @ 1 kHz (voice coil inductance @ 1 kHz) 2.549 Le @ 20 kHz (voice coil inductance @ 20 kHz) 0.674 Red @ Fs 0.81 Red @ 1 kHz 10.10 Red @ 20 kHz 99.48	mH
Le @ 1 kHz (voice coilinductance @ 1 kHz) 2.549 Le @ 20 kHz (voice coilinductance @ 20 kHz) 0.674 Red @ Fs 0.81 Red @ 1 kHz 10.10 Red @ 20 kHz 99.48 Krm 12.690	mH mH



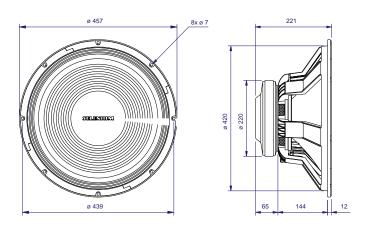
ADDITIONAL INFORMATION

Magnet material				E	Barium ferrite
Magnet weight			3,440	(120)	g (oz)
Magnet diameter x depth	20 x	24	(8.66 x	0.95)	mm (in)
Magnetic assembly weight		. 11	,200 (2	4.69)	g (lb)
Frame material					Aluminum
Frame finish					Black epoxy
Magnetic assembly steel finish					E-Coating
Voice coil material					. Flat CCAW
Voice coil former material					Fiberglass
Cone material		1	Non pre	ssed lo	ng fiber pulp
Volume displaced by woofer			. 8.6 (0	.304)	I (ft ³)
Net weight		. 14	,180 (3	1.26)	g (lb)
Gross weight		. 15	,400 (3	3.95)	g (lb)
Carton dimensions (W x D x H) 48 x 48 x	24 (18.9	9x 18.9	x 9.5)	cm (in)

MOUNTING INFORMATION

Number of bolt-holes	8	
Bolt-hole diameter	8 .0 (0.32)	mm (in)
Bolt-circle diameter	438 (17.24)	mm (in)
Baffle cutout diameter (front mount)	422 (16.61)	mm (in)
Baffle cutout diameter (rear mount)	412 (16.22)	mm (in)
Connectors	Silver-plated ρι	ish terminals
Polarity		
4.0	wasing I (woul) airea formeral	

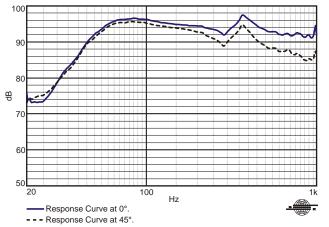
terminal (red) gives forward cone motion Minimum clearance between the back of the magnetic assembly and the



Dimensions in mm.

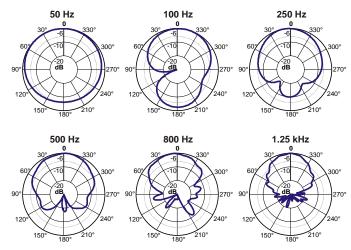
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RESPONSE CURVES (0° AND 45°) IN A TEST ENCLOSURE ON GROUND PLANE AND OUTDOOR ENVIRONMENT, 1 W / 1m



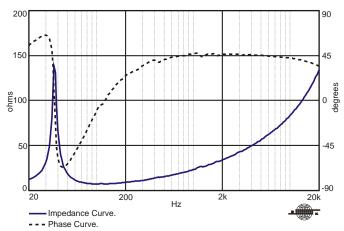
Response curves measured on ground plane and outdoor environment with the subwoofer installed in a test enclosure, 1 W / 1 m. This curves was decreased 6 dB to compensate the ground plane gain.

POLAR RESPONSE CURVES



Polar Response Curve.

IMPEDANCE AND PHASE CURVES, MEASURED IN FREE-AIR



HOW TO CHOOSE THE RIGHT AMPLIFIER

The power amplifier must be able to supply twice the RMS driver power. This 3 dB headroom is necessary to handle the peaks that are common to musical programs. When the amplifier clips those peaks, high distortion arises and this may damage the transducer due to excessive heat. The use of compressors is a good practice to reduce music dynamics to safe levels.

FINDING VOICE COIL TEMPERATURE

It is very important to avoid maximum voice coil temperature. Since moving coil resistance $(R_{\scriptscriptstyle E})$ varies with temperature according to a well known law, we can calculate the temperature inside the voice coil by measuring the voice coil DC resistance:

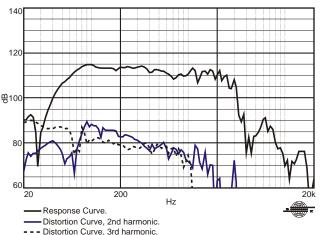
$$T_B = T_A = \frac{R_B}{R} = 1 \quad T_A = 25 \quad \frac{1}{R}$$

 T_A , T_B = voice coil temperatures in °C.

 R_A , R_B = voice coil resistances attemperatures T_A and T_B , respectively.

= voice coil wire temperature coefficient at 25 °C.

HARMONIC DISTORTION CURVES MEASURED AT 10% AES INPUT POWER IN A TEST ENCLOSURE INSIDE AN ANECHOIC CHAMBER, 1 m $\,$



POWER COMPRESSION

Voice coil resistance rises with temperature, which leads to efficiency reduction. Therefore, if after doubling the applied electric power to the driver we get a 2 dB rise in SPL instead of the expected 3 dB, we can say that power compression equals 1 dB. An efficient cooling system to dissipate voice coil heat is very important to reduce power compression.

NON-LINEAR VOICE COIL PARAMETERS

Due to its close coupling with the magnetic assembly, the voice coil in electrodynamic loudspeakers is a very non-linear circuit. Using the non-linear modeling parameters Krm, Kxm, Erm, Exm from an empirical model, we can calculate voice coil impedance with good accuracy.

SUGGESTED PROJECTS

HB1805A1 HB1805B1 HB1805C1 VB1805A1 PAS1G1 PAS2G1 PAS3G1

For additional project suggestions, please access our web site.

TEST ENCLOSURE

191-liter volume with 3 ducts ø 6" by 7.87" length.